

### FMI co-simulation 1D-3D SIMSEN-CFX

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## Co-Simulation 1D-3D

#### Interest : ۲

- Hydraulic systems may experience excitation caused by complex flow patterns within various components of the system
  - Characterization of the excitation source by 3D simulations
  - → System response with 1D compressible model
- Co-simulation of interest if strong interaction exists between excitation source and hydraulic system response in case of resonance or instability phenomena  $\rightarrow$  excitation source modified by the hydraulic system response





## Numerical Tools and Setup

- SIMSEN :
  - ✓ 1D differential equations of momentum and continuity for compressible fluid in pipes
  - ✓ Transient scheme is Runge-Kutta 4th order
    - → Explicit scheme
- CFX :
  - ✓ Reynolds Averaged Navier Stokes Equations
  - ✓ Fluid compressibility defined by barotropic law
  - ✓ Homogeneous ZGB cavitation model with heat transfer model as isothermal
  - ✓ SST turbulence model
  - ✓ Transient scheme is second backward Euler
    - → Implicit scheme with maximum of 10 internal coefficient loops
- ANSYS-CFX can run co-simulations (from 2021R2) using Functional Mock-up Interface (FMI) technology





## Water Hammer Case Study

 $CFL = \frac{a \cdot \Delta t}{\Delta t}$ 

- Pipe characteristics:
  - ✓ L = 480m, D = 0.5m,  $\lambda$  = 0.089
  - ✓ 2 parts: 1D and 3D
  - ✓ 3 wave speed combinations:
    - #1: a<sub>1D</sub> = a<sub>3D</sub> = 1'444 m/s
    - #2: a<sub>1D</sub> = a<sub>3D</sub> = 150 m/s
    - #3: a<sub>1D</sub> = 1'444 m/s & a<sub>3D</sub> = 150 m/s
- Co-simulation:
  - Between 1D pipe and 3D pipe & perturbation in the 3D domain
  - ✓ Time step simulation:  $dt_{#1} = 0.0015s$ ,  $dt_{#2} = 0.015s$  and  $dt_{#3} = 0.003 s$
  - $\checkmark$  No subcycling  $\Rightarrow$  exchanged data at each time step
  - ✓ 1D model :
    - L<sub>1D</sub> = 0.8L = 383m
    - Nb = 79  $\rightarrow$  dx = 4.85m
    - CFL<sub>#1</sub> = 0.446, CFL<sub>#2</sub> = 0.464, CFL<sub>#3</sub> = 0.969
  - ✓ 3D model :
    - L<sub>3D</sub> = 0.2L = 97m
    - dx = 0.4m
    - CFL<sub>#1</sub> = 5.411, CFL<sub>#2</sub> = 5.625, CFL<sub>#3</sub> = 1.125



Perturbation: static pressure elevation at the outlet of the 3D domain





## **Exchanged** Data





## Validation of co-simulation

- Comparison with the reference 1D SIMSEN simulation
  - → Pressure fluctuations in the middle of the pipe, i.e. in 1D domain

#1 : a<sub>1D</sub> = a<sub>3D</sub> = 1'444 m/s

#2 : a<sub>1D</sub> = a<sub>3D</sub> = 150 m/s

#3 : a<sub>1D</sub> = 1'444 m/s & a<sub>3D</sub> = 150 m/s



#### POWER VISION FNGINFFRING Vortex Shedding Resonance Case Study





Parameter	Symbol	Unit	Value
Pipe length	L	m	1.05
Pipe width	W	mm	40
Hydraulic diameter	$D_h$	mm	40
Wall thickness	e	$\mathbf{m}\mathbf{m}$	2
Position of bluff body	$x_{bb}/L$	-	0.75
Diameter of bluff body	D	mm	20
Cavitation free natural frequency	$f_n$	Hz	96.5
Measured cavitation incipience	$\sigma_i$	-	9
Reynolds number at pipe inlet	Re	-	60'000
Wave speed	a	m/s	202.65

- Resonance in square pipe due to von Karman vortex shedding
  - Cavitating condition or not with setup of vacuum pump
  - ✓ In non-cavitating condition resonance occurs with 1<sup>st</sup> pipe's eigenmode
  - $\checkmark$  In cavitating condition, resonance occurs with 2<sup>nd</sup> pipe's eigenmode
- Test case setup by Ruchonnet N. at EPFL (PhD N°4778 -2010) to validate coupled simulation without FMI protocol 7



## **Domains and Exchanged Data**





8



## Co-simulations Operating Conditions

#### • 4 co-simulations performed:

- Non-cavitating and out of resonance condition
- ✓ Non-cavitating and resonance condition
- $\checkmark$  Cavitating and out of resonance condition
- Cavitating and resonance condition
- Targeted resonance with :
  - ✓ 1st eigenmode in non-cavitating condition
  - 2nd eigenmode in cavitating condition which frequency is decreased due to cavitation

			1		2
[	Variable	Unit	Out of resonance		In resonance
Ē	С	m/s	3		2.54
	fs/fn	-	1.18		0.99
	St	-	0.38		0.38
	$\sigma_{corr}/\sigma_i$	-	1.96		1.40
-					
(		3	_	4	
Experimentally expected		1 Out of resonance		In resonance	
Found numerically as		s Near resonance		Out of resonance	
Variable Unit					
C m/s		3		3.27	
fs	$/f_n$	-	1.34		1.59
	St	-	0.43		0.47
$\sigma_{con}$	$r_r/\sigma_i$	-	0.84		0.78

 $St = \frac{f \cdot D}{C}$   $\sigma = \frac{p - p_v}{\frac{1}{2}\rho C^2}$ 

9

#### POWER VISION ENGINEERING Non-cavitating and out of resonance conditions<sup>1</sup>

Pressure coefficient fluctuations  $c_p'$  at L=L<sub>TOT</sub> = 0.5

Power spectrum density (PSD), time history and waterfall diagram



#### POWER VISION ENGINEERING Non-cavitating and resonance conditions<sup>1</sup>

Pressure coefficient fluctuations  $c_p'$  at L=L<sub>TOT</sub> = 0.5

Power spectrum density (PSD), time history and waterfall diagram



![](_page_11_Picture_0.jpeg)

# Non-cavitating and resonance conditions<sup>(2)</sup>

![](_page_11_Figure_2.jpeg)

- Comparison between co-simulation and CFD simulation without coupling :
  - ✓ No difference in velocity profile
  - ✓ Pressure pulsation due to resonance with 1D system with the co-simulation

![](_page_12_Picture_0.jpeg)

### Cavitating condition 3 4

Pressure coefficient fluctuations  $c_p'$  at L=L<sub>TOT</sub> = 0.5 Power spectrum density (PSD), time history and waterfall diagram

![](_page_12_Figure_3.jpeg)

![](_page_13_Picture_0.jpeg)

## Cavitating condition <sup>(3) (4)</sup>

#### Waterfall diagram of Power spectrum density (PSD)

![](_page_13_Figure_3.jpeg)

Bluff body position

f/fn

L/L<sub>tot</sub>

2

Bluff body position

L/L<sub>tot</sub>

Bluff body position

f1st eigen

 $f/f_n$  f2nd eigen

L/L tot

f1st eigen

f/fn

f2nd eigen

![](_page_14_Picture_0.jpeg)

### **Cavitating condition**

Pressure coefficient fluctuations  $c_p'$  at L=L<sub>TOT</sub> = 0.5 Power spectrum density (PSD), time history and waterfall diagram

![](_page_14_Figure_3.jpeg)

- Comparison between co-simulation and CFD simulation without coupling :
  - ✓ No difference in velocity profile
  - ✓ Pressure pulsation due to resonance with 1D system with the co-simulation is not visible like in non-cavitating condition since maximum amplitude of the eigenmode is located in the 1D domain (L/Ltot ≈ 0.4)

![](_page_15_Picture_0.jpeg)

## Conclusions

- FMI co-simulation between SIMSEN and CFX is now operational. Two case studies have been investigated to validate robustness of the FMI protocol :
  - Pressure wave propagation through the numerical domains
  - Resonance in cavitating condition with strong interaction between 1D model and 3D model including the excitation source
- Co-simulation could be of interest for any CFD simulations having unsteady and realistic boundary conditions driven by the 1D hydraulic system like surge tank device
- Co-simulation with SIMSEN could be extended to other physics like electromagnetics with Finite Element Analysis in electrical machines

![](_page_15_Figure_7.jpeg)

![](_page_15_Figure_8.jpeg)

![](_page_16_Picture_0.jpeg)

## Thank you for your attention!

![](_page_16_Picture_2.jpeg)

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![](_page_17_Picture_0.jpeg)

![](_page_17_Picture_1.jpeg)

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